

EFFECT OF THE PSEUDOTIME FUNCTION ON GAS RESERVOIR DRAINAGE AREA DETERMINATION

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The gas flow equation is normally linearized to allow the liquid solution of the diffusivity equation to satisfy gas behavior when analyzing transient test data of gas reservoirs. When wellbore storage conditions are insignificant, drawdown tests are best analyzed using the pseudopressure function. On the other hand, buildup pressure tests require linearization of both pseudotime and pseudopressure. It is not the case for the *TDS* technique which is indifferently applied to either drawdown or buildup tests. However, whichever the case, pseudotime has certain effect at very long testing times in formations of moderate to high permeability.

In this paper, we implemented the Tiab's Direct Synthesis (*TDS*) technique, to include pseudotime effects, and observe its influence on the interpretation results of gas well test data at early and late time periods. New analytical equations to estimate reservoir permeability, wellbore storage coefficient, pseudoskin factor and reservoir drainage area are presented. Then, a comparison of results against rigorous time was carried out for simulated and field cases. We found acceptable results for permeability, pseudoskin factor and wellbore storage coefficient. However, for the case of reservoir drainage area, the deviation error was of 4,1% for a simulated case and 17,9% for a field case. However, the smaller of these deviations may be small if related to pressure transient analysis results. However, this deviation in a gas reservoir with reserves of one tera standard cubic feet is equivalent to a huge difference of 38 gigas of standard cubic feet of gas which may have an economic impact to any oil company.

Keywords: reservoir gas, pressure, *TDS* technique, steady state, permeability, radial flow, mathematical models.

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Normalmente, la ecuación de flujo de gas se linealiza para permitir que la solución de difusividad de los líquidos satisfaga el comportamiento del gas cuando se analizan pruebas de presión en yacimientos gasíferos. Las pruebas de declinación de presión se analizan mejor usando la función pseudopresión, cuando los efectos de almacenamiento de pozo son insignificantes. Por otra parte, las pruebas de restauración de presión requieren la linealización tanto de la pseudopresión como del pseudotiempo. Sin embargo, cualquiera que sea el caso, la función de pseudotiempo presenta ciertos efectos a tiempos de prueba muy largos en formaciones de permeabilidad moderada a alta.

En este artículo, implementamos la técnica de Síntesis Directa de Tiab, (*TDS*), para incorporar los efectos del pseudotiempo, y observar su influencia en los resultados de interpretación de pruebas de presión en yacimientos de gas a tiempos tempranos y tardíos. Se desarrollaron nuevas ecuaciones analíticas para la estimación de la permeabilidad del yacimiento, el coeficiente de almacenamiento del pozo, el factor de pseudodaño y el área de drenaje del pozo. Luego, para casos de campo y simulados, se efectuó una comparación de los resultados contra aquellos donde se usa el tiempo riguroso o normal. Encontramos valores aceptables de permeabilidad, pseudo factor de daño y coeficiente de almacenamiento. Sin embargo, para el área de drene del pozo, la desviación fue de 4,1 y de 17,9% para un caso de campo. La menor de estas desviaciones es un número que resulta pequeño si lo relacionamos con los resultados producidos en la interpretación de pruebas de presión. Sin embargo, esta desviación en un yacimiento con reservas de un tera de pies cúbicos a condiciones normales equivale a una enorme diferencia de 38 gigas de pies cúbicos a condiciones normales lo cual puede impactar económicamente a cualquier empresa.

Palabras clave: yacimientos de gas, presión, técnica *TDS*, estado estacionario, permeabilidad, flujo radial, modelos matemáticos.

NOMENCLATURE

A	Drainage area, ft ²
B	Oil volume factor, bbl/STB (crude), bbl/Mpcn (gas)
C	Wellbore storage coefficient, bbl/psi
D	Non-Darcy flow coefficient, (Mscf/D) ⁻¹
c	Compressibility, 1/psi
c_t	Total compressibility, 1/psi
h	Formation thickness, ft
k	Permeability, md
$m(p)$	Pseudopressure function, psi ² /cp
p	Pressure, psi
q_g	Gas flow rate, Mscf/D
r_w	Well radius, ft
s	Skin factor
s'	Pseudoskin factor
T	Temperature, °R
t	Time, h
$t_a(p)$	Pseudotime function, psi h/cp
$t^*\Delta m(p)'$	Pseudopressure derivative function with respect to rigorous/real time
$t_a^*\Delta m(p)'$	Pseudopressure derivative function with respect to pseudotime
Z	Gas deviation factor

GREEK

Δ	Change, drop
\emptyset	Porosity, fraction
μ	Viscosity, cp

SUBINDEXES

D	Dimensionless
e	external
g	gas
i	Intersection or initial conditions
L	Linear
pss	Pseudosteady state
r	radial flow
rpi	Intersection between radial and pseudosteady state lines
sc	Standard conditions
t	Total
w	Well

S.I. METRIC CONVERSION FACTORS

Bbl x 0,1589873	= m ³
cp x 0,001	= Pa.s
ft x 0,3048	= m
ft ² x 0,09290304	= m ²
psi x 6,894 757	= KPa
Ac. x 4046,856	= m ²

INTRODUCTION

A very important concept to account for gas flow behavior was introduced by Al-Hussainy, Ramey, and Crawford (1966). This was called the pseudopressure function which basically includes the variation of both gas viscosity and compressibility factor which are combined into a single function. Since the dimensionless time involves the viscosity-compressibility product which, for gases, is a function of pressure, then, Agarwal (1979) developed the pseudotime function and performed a practical application to pressure buildup test in vertical fractured wells. Besides Agarwal (1979), Lee and Holditch (1982) demonstrated the advantages of using the pseudotime function in pressure buildup testing of tight formations.

Graham and Warwick (1984), proposed a new formulation called scale-time which is only function of time rather than the function of both time and position as previously defined by Agarwal (1979). They demonstrated easier mathematical manipulations but did not provide practical advantages related to well tests.

Later, Spivey and Lee (1986) found the necessity of applying the pseudotime function to linearize the equations under prevalent conditions of wellbore storage during the interpretation of pressure buildup tests and use both pseudotime and pseudopressure for drawdown cases. They utilized type-curve matching for well test interpretation purposes.

To simplify the estimation of the pseudotime function, Aminiam, Ameri, Abbitt, and Cunningham (1991) presented an analytical expressions with the aid of polynomial regression analysis so that the pseudotime

function could be easily estimated. They found a deviation of 0,3% which is an adequate range for engineering applications.

In this work, the application of the pseudotime function concept is applied to further extend the application scope of the *TDS* technique. The study presents new analytical equations for reservoir permeability, pseudoskin factor, wellbore storage coefficient and reservoir drainage area as a function of the pseudotime function. Afterwards, both field and numerical examples were used to test the variation of the above named parameters obtained from the solutions of this study and compared against the solution using actual time, as proposed by Nuñez, Tiab, and Escobar (2002, 2003). It was found that the reservoir drainage area was affected more than the remaining parameters (permeability, pseudoskin factor and wellbore storage coefficient) which impact was irrelevant.

MATHEMATICAL DEVELOPMENT

Agarwal (1979) introduced the pseudotime function to account for the time dependence of gas viscosity and total system compressibility:

$$t_a = \int_{t_0}^t \frac{dt}{\mu(t)c_i(t)} \quad (1)$$

Pseudotime is better defined as a function of pressure as a new function given in h psi/cp:

$$t_a(p) = \int_{p_0}^p \frac{(dt/dp)}{\mu(p)c_i(p)} dp \quad (2)$$

Notice that μ and c_t are now pressure dependent properties. In their analysis for the application of the TDS technique of gas reservoirs, Nuñez *et al.* (2003) used the following dimensionless quantities:

$$t_D = \frac{0,0002637kt}{\phi(\mu c_t)_i r_w^2} \quad (3)$$

$$m(p)_D = \frac{hk[m(p_i) - m(p)] T_{sc}}{50320,54q_{sc} T p_{sc}} \quad (4)$$

$$C_D = \left(\frac{0,8935}{\phi h c_t r_w^2} \right) C \quad (5)$$

Including the pseudotime function, $t_a(p)$, in Equation 3, the dimensionless pseudotime is given by:

$$t_{Da} = \left(\frac{0,0002637k}{\phi r_w^2} \right) t_a(p) \quad (6)$$

Notice that the viscosity-compressibility product is not seen in Equation 4 since they are included in the pseudotime function. However, if we multiply and, then, divide by $(\mu c_t)_i$ a similar equation to the general dimensionless time expression, Equation 3, will be obtained.

$$t_{Da} = \left(\frac{0,0002637k}{\phi(\mu c_t)_i r_w^2} \right) [(\mu c_t)_i \times t_a(p)] \quad (7)$$

As presented by Tiab (1993, 1995), the governing equation for the well pressure behavior during radial flow is expressed by:

$$m(p)_{Dr} = \left(\frac{7,029 \times 10^{-4} kh}{qT} \right) \left(\frac{m(p_i) - m(p_{wf})}{q_n} \right) = \frac{1}{2} (\ln t_D + 0,80907 + 2s) \quad (8)$$

From a log-log plot of pseudopressure and pseudopressure derivative against pseudotime, Figure 1, several main characteristics are outlined;

1. The early unit-slope line originated by wellbore storage is described by the following equation:

$$m(p)_D = \frac{t_{Da}}{C_D} \quad (9)$$

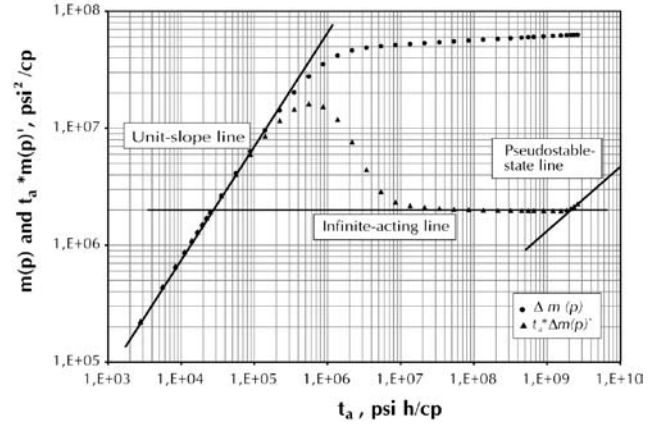


Figure 1. Log-log plot of pseudopressure and pseudopressure derivative vs. pseudotime

Replacing the dimensionless parameters in Equation 9, a new equation to estimate the wellbore storage coefficient is obtained:

$$C = (0,419qTc_t) \left(\frac{t_a(p)}{\Delta m(p)_q} \right) \quad (10)$$

2. The intersection of the early unit-slope line with the radial horizontal straight line gives:

$$\left(\frac{t_{Da}}{C_D} \right)_i = 0,5 \quad (11.a)$$

From the above relationship is obtained an equation to estimate either permeability or wellbore storage once the dimensionless parameters are replaced:

$$t_a(p)_i = \frac{1695c_t C}{kh} \quad (11.b)$$

3. According to Tiab (1993, 1995), another form of Equation 8 is obtained when wellbore storage and skin factor are included:

$$m(p)_{Dr} = \frac{1}{2} \left\{ \ln \left(\frac{t_{Da}}{C_D} \right)_r + 0,80907 + \ln (C_D e^{2s}) \right\} \quad (12)$$

From the above equation, the derivative of pseudopressure with respect to $\ln t_{Da}/C_D$:

$$\left[\frac{t_{Da}}{C_D} m'(p)_D \right]_r = 0,5 \quad (13)$$

From Equation 4, the dimensionless pseudopressure derivative with respect to $\ln t_{Da}/CD$ gives:

$$\left[\frac{t_{Da}}{C_D} m'(p)_D \right]_r = \left[7,029 \times 10^{-4} \frac{kh}{qT} \right] [t_a(p) * m'(p)] \quad (14)$$

Combination of Equation 12 and Equation 13 will result into an equation to estimate permeability:

$$k = \frac{711.26qT}{h[t_a(p) * \Delta m'(p)]} \quad (15)$$

4. Dividing Equation 11.a by Equation 12, replacing the dimensionless quantities in the resulting expression and, then, solving for the pseudoskin factor will yield:

$$s' = 0,5 \left[\frac{(\Delta m(p)_q)_r}{[t_a(p) * \Delta m(p)]_r} - \ln \left(\frac{k(t_a(p))_r}{\phi r_w^2} \right) + 7,4316 \right] \quad (16)$$

The pseudosteady state solution of the diffusivity equation of closed systems is expressed by:

$$m(p)_D = 2\pi t_{Da} + \ln r_{eD} - \frac{3}{4} \quad (17.a)$$

As suggested by Equation 17.a, the analysis in this work is only applicable for circular drainage areas, then, we have to consider limitations to other reservoir shapes. The pseudopressure derivative of the above equation is then:

$$t_{Da} * m'(p)_D = 2\pi t_{Da} \quad (17.b)$$

The intersection point of the above straight line and the radial flow line is:

$$(t_a)_{DArpi} = \frac{1}{4\pi} \quad (18)$$

After substituting the dimensionless pseudotime function into Equation 18, a new equation for the well drainage area is presented:

$$A = \frac{kt_a(p)_{pss}}{301,77 \phi} \quad (19)$$

For comparative purposes, we cite the following equations developed by Nuñez *et al.* (2003).

$$k = \frac{711,26qT}{h[t * \Delta m'(p)]_r} \quad (20)$$

$$s' = 0,5 \left[\frac{(\Delta m(p)_q)_r}{[t * \Delta m(p)]_r} - \ln \left(\frac{kt_r}{\phi r_w^2} \right) + 7,4316 \right] \quad (21)$$

$$C = \left(0,419 \frac{qT}{\mu_i} \right) \left(\frac{t}{\Delta m(p)} \right) \quad (22)$$

The following equation is taken from Nuñez *et al.* (2002).

$$A = \frac{kt}{301,77 \phi \mu c_{ii}} \quad (23)$$

STEP-BY-STEP PROCEDURE

Detailed explanation of the appropriate use and application of the TDS technique are presented by Tiab (1993, 1995), Tiab (1993, 1994), Nuñez *et al.* (2002), Nuñez *et al.* (2003). A summarized procedure is outlined as follows:

Step 1. Construct a log-log plot of $\Delta m(p)$ and $t_a * \Delta m(p)'$ versus t_a .

Step 2. Identify the different flow regimes and draw the horizontal line along both radial flow and the unit-slope line. For the later case, the line is drawn through both the wellbore storage points and the late pseudosteady-state regime, if given the case.

Step 3. Read the intersection point of the wellbore storage line and the radial flow line, $(t_{aip}, \Delta m(p)_i)$, note that: $\Delta m(p)_i = (t_a * \Delta m(p))'_i = (t_a * \Delta m(p))'_r$, and find the wellbore storage coefficient from Equation 10 and the permeability from Equation 15. Permeability ought to be verified with Equation 11.b using the pseudotime of intersection of the early unit-slope and the radial lines.

Step 4. Select any convenient pseudotime during radial flow, $t_a(p)_r$, and read the corresponding $\Delta m(p)_r$ value, then, determine the pseudoskin factor, s' , using Equation 16.

Step 5. Read the intersection pseudotime, $t_a(p)_{pss}$, of the late pseudosteady-state flow regime and the horizontal straight line and determine reservoir drainage area with Equation 19.

EXAMPLES

Field example 1

Lee (1982) presented a drawdown test ran in a gas reservoir. The reservoir, gas and well data are given in Table 1. It is required to estimate reservoir permeability, pseudoskin factor, and wellbore storage coefficient using the *TDS* technique for both real time and pseudotime.

Solution

Once the pseudopressure and pseudotime were estimated, Figures 2a and 2b were constructed. An average radial flow line was drawn. The chosen points read from these plots were:

$$t_i = 0,01 \text{ h (36 s)}$$

$$t_a(p)_i = 1\,000 \text{ psi h/cp (2 482} \cdot 10^{13} \text{ s KPa/Pa} \cdot \text{s)}$$

$$\Delta m(p)_i = (t_a \cdot \Delta m(p)')_i = (t_a \cdot \Delta m(p)')_r = 5'510,526 \text{ psi}^2/\text{cp (2,620} \cdot 10^{11} \text{ KPa}^2/\text{Pa} \cdot \text{s)}$$

$$t_a(p)_r = 247\,402,7 \text{ psi h/cp (6,141} \cdot 10^{12} \text{ s KPa/Pa} \cdot \text{s)}$$

$$t_r = 2,015 \text{ h (7254 s)}$$

$$\Delta m(p)_r = 54'119\,360 \text{ psi}^2/\text{cp (3,520} \cdot 10^{12} \text{ KPa}^2/\text{Pa} \cdot \text{s)}$$

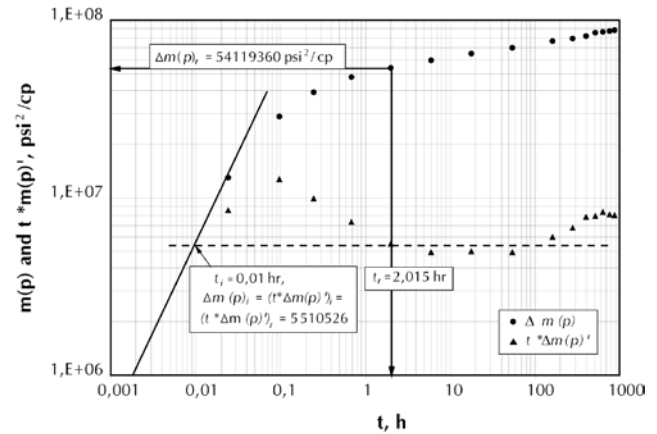


Figure 2a. Log-log plot of pseudopressure and pseudopressure derivative vs. time for the field example 1

Using *Equation 15*, *10* and *16*, permeability of 8,519 md, wellbore storage coefficient of 0,012 Mscf/psi (0,04928 m³/KPa) and pseudoskin factor of -0,71 were respectively estimated. These same parameters, see Table 2, were also found for the actual time using *Equations 20*, *21* and *22*. Table 2 displays the results of interpreting the test by means of non-linear regression analysis using a commercial software. We are not satisfied with these results because of poor matching

Table 1. Reservoir, gas and well properties for the worked examples

	FIELD EXAMPLE 1	FIELD EXAMPLE 2	FIELD EXAMPLE 3	SIMULATED EXAMPLE 1	SIMULATED EXAMPLE 2
Paramater	Value				
p_i , psia	3000	7800	1062	4500	5000
k , md	8,51 ⁽¹⁾	0,13 ⁽²⁾	-	10	30
S'	-1,42 ⁽²⁾	3,5 ⁽²⁾	-	5	-
C , Mscf/psi	0,0247 ⁽³⁾	0,1 ⁽²⁾	-	2	-
T , °R	660	705	570	672	672
q_{gr} Mscf/D	1000	415	10000	5000	5000
h , ft	10	14,5	40	100	50
ϕ , %	19	12,5	16	5	5
c_{li} , 1/psi	$2,35 \cdot 10^{-3}$	$6,45 \cdot 10^{-4}$	0,00103	$1,18 \cdot 10^{-4}$	$1,32 \cdot 10^{-4}$
μ_i , cp	0,02024	0,0306	0,013	0,03036	0,026647
γ_g		0,65	0,58	0,9	0,7
r_w ft	0,365	0,3	0,3	0,3	0,3
A , Ac	-	-	-	14 128	-

(1) Determined by non-linear regression analysis from a commercial software
 (2) From Spivay and Lee (1986)

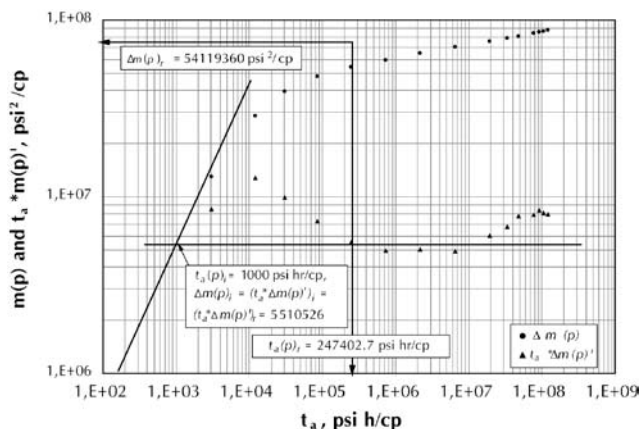


Figure 2b. Log-log plot of pseudopressure and pseudopressure derivative vs. pseudotime for the field example 1

between the actual pressure trend and the simulated solution.

Field example 2

Spivey and Lee (1986) presented a drawdown test ran in a gas reservoir. The relevant information

for this test is reported in Table 1. Estimate reservoir permeability, pseudoskin factor, and wellbore storage coefficient using the TDS technique for both real time and pseudotime.

Solution

From the pseudopressure and pressure derivative plots, Figures 3a and 3b the following data are read:

$$t_i = 0,162 \text{ h (583,2 s)}$$

$$t_a(p)_i = 81\,129,7 \text{ psi h/cp (2,014} \cdot 10^{12} \text{ s KPa/Pa-s)}$$

$$\Delta m(p)_i = (t_a * \Delta m(p))_i = (t_a * \Delta m(p))_r = 118'338\,700 \text{ psi}^2/\text{cp (5,626} \cdot 10^{12} \text{ KPa}^2/\text{Pa-s)}$$

$$t_a(p)_r = 50'269\,174,4 \text{ psi h/cp (1,248} \cdot 10^{15} \text{ s KPa/Pa-s)}$$

$$t_r = 350,9 \text{ h (1,26} \cdot 10^6 \text{ s)}$$

$$\Delta m(p)_r = 3\,670'356\,000 \text{ psi}^2/\text{cp (1,745} \cdot 10^{14} \text{ KPa}^2/\text{Pa-s)}$$

Table 2. Results of the worked examples

	REAL TIME	PSEUDOTIME	SIMULATOR	ABS. DEVIATION WITH RESPECT PSEUDOTIME
Field Example 1				
Parameter				
k , md	8,52	8,519	8,51	-0,01
S'	-0,1	-0,71	-1,42	85,48
C , Mscf/psi	0,02	0,012	0,0247	86,85
Field Example 2				
k , md	0,12	0,12	0,13	0,00
S'	8,54	9,17	3,50	6,85
C , Mscf/psi	0,01	0,0054	0,10	-84,36
Field Example 3				
k , md	1366	1356	1310	0,73
S'	1,33	1,39	7,3	4,31
A , Ac	388	329	336	17,93
Simulated Example 1				
k , md	12,481	12,481	10	0,00
S'	5,284	5,311	5	0,51
C , Mscf/psi	2,180	2,180	2	0,01
Simulated Example 2				
A , Ac	14 670,9	14 093,2	14 128,4	4,10

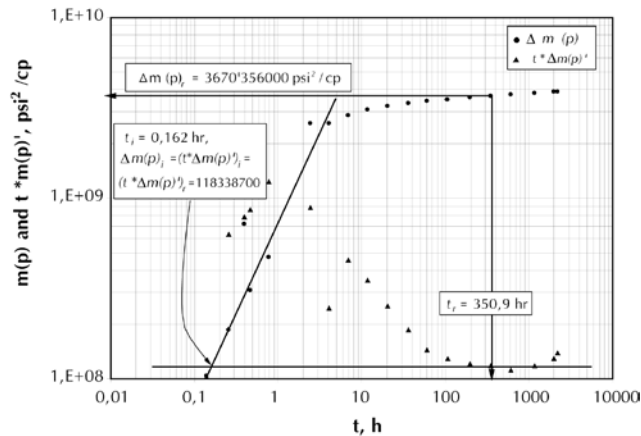


Figure 3a. Log-log plot of pseudopressure and pseudopressure derivative vs. time for the field example 2

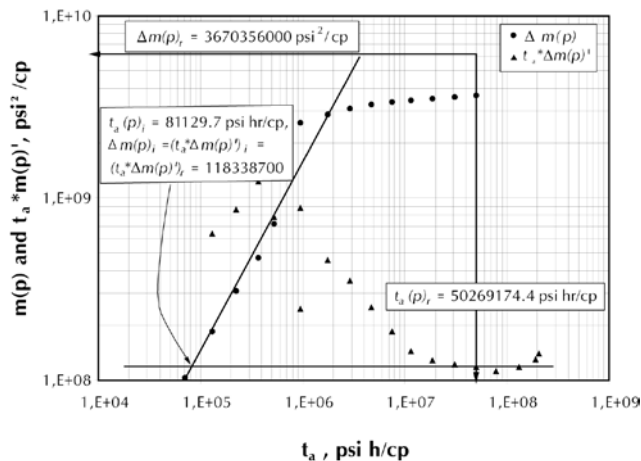


Figure 3b. Log-log plot of pseudopressure and pseudopressure derivative vs. pseudotime for the field example 2

Using Equation 15, 10 and 16, permeability of 8,52 md, wellbore storage coefficient of 0,0054 Mscf/psi (0,02218 m³/KPa) and pseudoskin factor of -0,71 were respectively estimated. Same calculations were performed with using Equation 20 through Equation 22, as reported in see Table 2. That table presents not only the results from this study but also those from Spivay and Lee (1986) which were found by type-curve matching.

Field example 3

A drawdown test was run in a unique well of a Colombian reservoir with pseudopressure and pseudopressure derivative reported in Figure 4a. Information concerning well, fluid and reservoir characteristics required for this test are given in Table 1 along with the other examples. Estimate reservoir permeability,

pseudoskin factor, and reservoir area with the TDS technique for both real time and pseudotime.

Solution

The pseudopressure and pressure derivative plots are given in Figures 4a and 4b for real time and pseudotime, respectively. The following data are read:

$$t_r = 1,97 \text{ h (7 092 s)}$$

$$\Delta m(p)_r = 1'370\,865 \text{ psi}^2/\text{cp (6,517} \cdot 10^{10} \text{ KPa}^2/\text{Pa} \cdot \text{s)}$$

$$(t_a * \Delta m(p)')_r = 74\,203 \text{ psi}^2/\text{cp (3,572} \cdot 10^9 \text{ KPa}^2/\text{Pa} \cdot \text{s)}$$

$$t_{rpi} = 8 \text{ h (2 800 s)}$$

$$t_a(p)_r = 100\,888 \text{ psi h/cp (2,504} \cdot 10^{12} \text{ sec KPa/Pa} \cdot \text{s)}$$

$$\Delta m(p)_r = 1'368\,609 \text{ psi}^2/\text{cp (6,506} \cdot 10^{10} \text{ KPa}^2/\text{Pa} \cdot \text{s)}$$

$$(t_a * \Delta m(p)')_r = 74\,750 \text{ psi}^2/\text{cp (3,553} \cdot 10^9 \text{ KPa}^2/\text{Pa} \cdot \text{s)}$$

$$t_a(p)_{rpi} = 510\,000 \text{ h (1,266} \cdot 10^{13} \text{ s KPa/Pa} \cdot \text{s)}$$

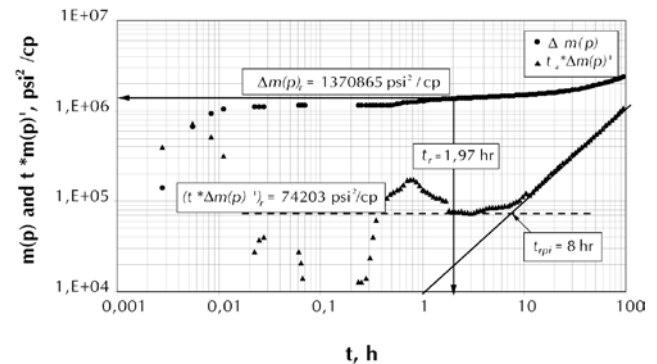


Figure 4a. Log-log plot of pseudopressure and pseudopressure derivative vs. time for the field example 3

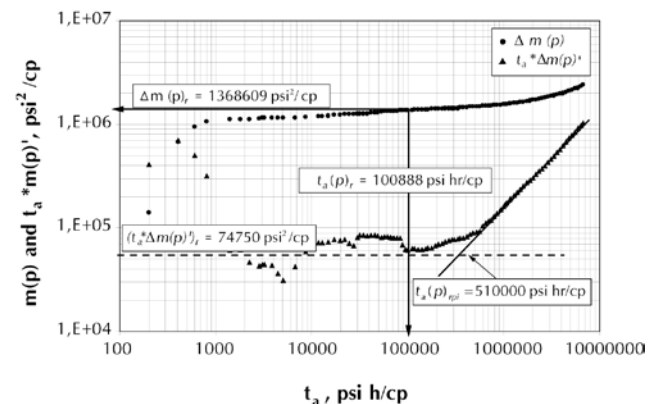


Figure 4b. Log-log plot of pseudopressure and pseudopressure derivative vs. pseudotime for the field example 3

A permeability of 1366 md, pseudoskin factor of 1,33 and reservoir drainage area of 388Ac were determined using *Equation 15, 16 and 19*, respectively. Besides these, Table 2 also contains the results for the same computations performed using *Equations 10, 23 and 21*, respectively, of Nuñez *et al.* (2002).

Simulated example 1

A pressure drawdown test in gas reservoir was simulated using a commercial software with the information of Table 1. Estimate for this system: permeability, pseudoskin factor and wellbore storage coefficient using the *TDS* technique with both actual time and pseudotime.

Solution

Pseudopressure and pseudopressure derivative are plotted against both actual time in Figure 5a and pseudotime in Figure 5b. The chosen points were:

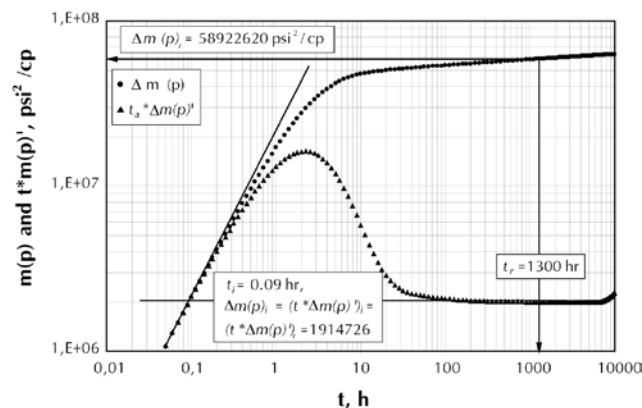


Figure 5a Log-log plot of pseudopressure and pseudopressure derivative vs. time for the synthetic example 1

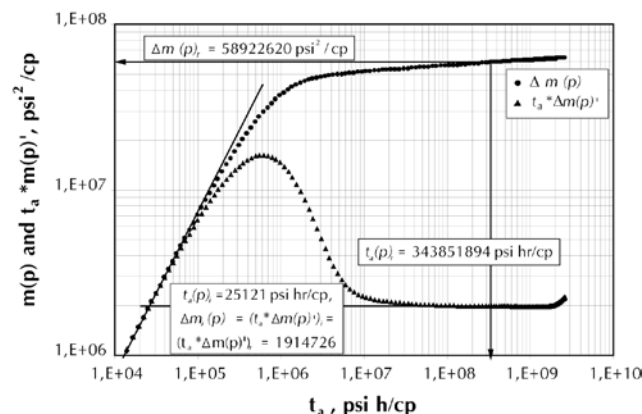


Figure 5b Log-log plot of pseudopressure and pseudopressure derivative vs. pseudotime for the synthetic example 1

$$t_i = 0,1 \text{ h (360 s)}$$

$$t_a(p)_i = 25 \text{ 121 psi h/cp (6,235*10}^{11} \text{ s KPa/Pa.s)}$$

$$\Delta m(p)_i = (t_a * \Delta m(p)')_i = (t_a * \Delta m(p)')_r = 1'914,726 \text{ psi}^2/\text{cp (9,102*10}^{10} \text{ KPa}^2/\text{Pa.s)}$$

$$t_a(p)_r = 343'851 \text{ 894 psi h/cp (8,535*10}^{15} \text{ s KPa/Pa.s)}$$

$$t_r = 1 \text{ 300 h (4,68*10}^6 \text{ s)}$$

$$\Delta m(p)_r = 58'922 \text{ 620 psi}^2/\text{cp (2,801*10}^{12} \text{ KPa}^2/\text{Pa.s)}$$

From *Equation 15* a permeability of 12,48 md was determined. It was also estimated a pseudoskin factor of 5,31 with *Equation 16* and a wellbore storage coefficient of 2,18 Mscf/psi (8,953 m³/KPa) with *Equation 10*. Practically the same results were obtained using *Equations 28.b, 18 and 28.c* from the reference of Nuñez *et al.* (2003).

Simulated example 2

A pressure drawdown test in a closed circular gas reservoir was also simulated using a commercial software based upon the information of Table 1. Estimate the area of this reservoir using the *TDS* technique and compare to the reference area given in Table 1.

Solution

The simulated values of pseudopressure and pseudopressure derivative against either real time or pseudotime are presented in Figures 6a and 6b, respectively. The intersection point of the radial and late pseudosteady-state lines is found at a pseudotime, $t_a(p)_{pri}$, of 308'763 737,3 h psi/cp (7,664*10¹⁸ s KPa/Pa.s) and the corresponding real intersection time, t_{pri} , is found to be 1133 hours (4,076*10⁶ s) from Figure 4b. The area with the rigorous time using *Equation 23* was of 14 670,9 Ac. (5,938*10⁸ m²). From *Equation 19* the estimated area was 14 093 Ac. (5,704*10⁸ m²).

ANALYSIS OF RESULTS

It is observed, from the worked examples, a good agreement between the simulated values of permeability, pseudoskin factor and wellbore storage obtained

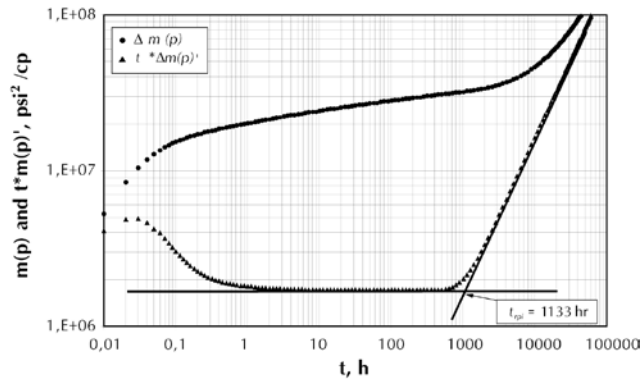


Figure 6a. Log-log plot of pseudopressure and pseudopressure derivative vs. time for the synthetic example 2

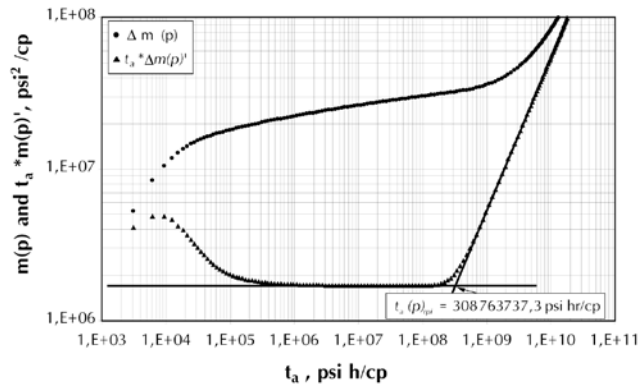


Figure 6b. Log-log plot of pseudopressure and pseudopressure derivative vs. pseudotime for the synthetic example 2

using the *TDS* technique when using either regular time or pseudotime. Practically, same values of permeability, pseudoskin factor and wellbore storage are found no matters if either rigorous time or pseudotime is utilized. However, as expected and exposed formerly in the literature, the estimation of the reservoir drainage area has a higher deviation resulting from the use of real time. The resulting drainage area using real time has an absolute deviation of 4,1% while the one with pseudotime has a deviation of 3,84% with respect to the simulated value. Also the deviation of the area when employing pseudotime has a deviation of 0,25% with respect to the simulated value. From field example 3 was found that the drainage area has an absolute deviation of 17,9% which is more remarkable. This confirms that the influence of pseudotime is more relevant for long producing times. Although, the deviation value

of 3,84% may fall into a widely accepted range of the daily measurements normally obtained from well test analysis, this can introduce significant differences in estimation of reserves.

The non-linear regression analysis simulation conducted using a commercial software did not match perfectly the pseudopressure and pressure derivative curve, therefore, the results may not be as accurate as expected. Consequently, the field cases were not treated in the analysis. Nonetheless, the results of the permeability reference values agree quite well with those from the *TDS* technique.

CONCLUSIONS

- Estimation of the drainage area in gas bearing formations is affected when the time is used rigorously. We found absolute differences between 4,1 and 17,9% which impacts also gas reserves. Therefore, to assure accuracy, care should be taken into account when interpreting long drawdown pressure tests. For either relatively short drawdown tests or highly low permeability gas formations, regular time may be used for practical purposes without incurring in a significant error.
- Additionally, the *TDS* technique has been extended by incorporating new analytical solutions, which include the pseudotime function, for the estimation of formation permeability, pseudoskin factor, wellbore storage coefficient and reservoir drainage area. Field and synthetic examples were carried out to test the sensitivity of the mentioned parameters when the pseudotime function is included, as compared to the actual time.

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